

Dipartimento di Ingegneria "Enzo Ferrari"

Progettazione Assistita di Organi di Macchine

Sara Mantovani sara.mantovani@unimore.it

Agenda

MSC Marc Mentat: Select entities

- Method & Mode;
- Store;
- Identify set.

Thin-walled profile in torsion

- Opened vs closed cross-section;
- Mesh convergence.

References

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MENU: SELECT

DRAW

PLOT

FILES

FILI

VIEW

VIEW

MODEL

RESET

DYN.

 $TX+$

 $TX -$

 $TY+$

 $TY-$

 $TZ+$

 $TZ -$

 $RX+$

 $PX-$

 $RY+$

 $RY-$

 $RZ+$

 $PZ-$ Ready | TN

OUT

SETTINGS HELP

This menu contains commands for selecting model entities and for creating sets of entities.

This menu is located on the bottom right-hand side of the Mentat windows *e.g.* MESH GENERATION.

Enter select element list Enter select element list all_selected

*invisible_selected

MEEX Softwar

MENU: SELECT

Select entities *e.g.* nodes, elements, points, curves, …

Select entities: METHOD *e.g.* nodes, elements, points, curves, …

SINGLE: this method allows the user to select entities singly by specifying their *IDs* or by manual selection (mouse). This method is the *default method.*

PATH: this method allows the user to select connected nodes or points along a path from the first entity specified to the last. You may specify only the beginning and end of the path, or choose entities at various location along the path.

BOX: this method allows the user to select items within a specified region in space therefore a volume assessed by coordinates. All items that fall within the specified box (global coordinate system) become selected.

Select entities: MODE *e.g.* nodes, elements, points, curves, …

AND: adopting this mode, additionally selected entities are added with those already in the selected list, thus adding them to the list. This mode is the *default mode.*

EXCEPT: by this mode, additionally selected entities are removed from the list of selected entities.

INVERT: in this mode, additionally selected entities are added to the list of selected entities if they do NOT belong to it and are removed if they do already belong to it.

INTERSECT: in this mode, additionally selected entities are intersected with the current list of selected entities to form the new list.

 \rightarrow I suggest you to do some exercises!!!!

RETURN

MAIN

Select entities: STORE *e.g.* nodes

Marc Mentat 2013.1.0 (64bit) (OpenGL): model3.mud

SELECT

Once nodes *(or elements, or edges, or faces, …)* are selected, they might be **stored** in a set with a

prescribed named.

Select entities: IDENTIFY SETS *e.g.* nodes

identification of set identifiers of all sets in the

e.g. the nodes of this quadrilateral elements are store in a set called *crucial_nodes* identified by

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GOAL:

Open the reference model named torsione rev01 nolabile.mud this profile is characterized by a lateral crack (open-cross section). It is loaded on the free extremity by an imposed rotation.

Starting from this model, we will compare the response of the open section profile with the homologous closed profile calculating their torsional stiffness.

torsione rev01 nolabile open vs close.mud

MESH GENERATION Duplicate

Duplicate Combined

The reference model will be **completely** duplicated (*e.g.* nodes, elements, BCs, links) , it will be located at a distance of 100 mm from the origin (0,0,0) along X-direction referring to the global coordinate system of the model.

Sweep

The left-hand side model is the profile with the open cross-section, named OPENED

The right-hand side model is the profile with the open cross-section, named CLOSED.

Therefore, the lateral crack of the right-hand side model will be removed by the SWEEP NODES function as shown here. Finally, the model is ready to be calculated (SUBMIT).

all selected **SWEEP** *select clear **JEEE** -----------------------TOLERANCE CHECK THE COMMAND PROMPT Deleting 3 duplicate nodes! MODE **V MERGE** SETE Deleting 0 collapsed elements! ELEMENTS NODES **CURVES** POINTS **SURFACES** ALL SUBMIT MODEL --------------------------------REMOVE UNUSED *check job POINTS **NODES** update job *submit job 1 **INVISIBLE ISIBLE** ALL FREE NDS ALL FREE NDS *monitor job ALL FREE PNTS ALL FREE PNTS save model ADVANCED PROJECTION SETTINGS **SELECT RETHEN MATN** INDC $TX+$ $TY+$ $TZ+$

SWEEP NODES - CLOSE LATERAL CRACK the tolerance (t) must be:

at least upper then the crack size; | lower than the elements size; therefore $0.1 < t < 20$

*set sweep tolerance

*sweep nodes

 0.2

| I consider a tolerance value equal to 0.2

Open the results file. Check if the **deformation** of the models is coherent with you expected!!!

Check the warping of the profile cross-section at their free extremity!! The simplest way is monitoring the displacement of the section along the Z direction (Displacement Z).

OPENED PROFILE: the maximum (minimum) Z-displacement is equal to 4.483 mm (-4.483 mm); CLOSED PROFILE: the maximum (minimum) Z-displacement is equal to 0.57 mm (-0.57 mm).

Moving from a opened to a closed section, the warping decreases significantly.

Check the warping of the profile cross-section at their free extremity!! The simplest way is monitoring the displacement of the section along the Z direction (Displacement Z). Some regions evidence a null deformation along the Z direction; therefore; along this segments, the warping does not occur.

Check if the **rotation along the Z axis (Rotation Z)** of the models is coherent with you expected!!! The models do not rotate at the skew symmetry plane (Z=0), and the maximum rotation is equal to 0.04 radians, and it is located at the free extremity of the model.

Collect the values of **Reaction Moment Z** to compare the stiffness of the two profiles accounting the influence of the lateral crack.

For the same rotation, the reaction moment increases moving from an opened to a closed section profile. Therefore, the torsional stiffness will be increased significantly, too.

04/04/2019

files has been analytically calculated oach for the closed section, and the in section under torsion.

re compared to the FE results, under the ing of the structures.

ss evaluation paom2019 v001.ods; ion property dz 40

ez. Sottili aperte

The maximum equivalent Von Mise stress occuring across the layers (top, middle, bottom) is plotted, and the opened and the closed profiles achieve the maximum stress value equal to 93 MPa and 1434 MPa, respectively.

op/front op/front/inside on/hack/outside

From the analysis of the components of stress at the TOP SURFACE, the stress that contributes significantly to the evaluation of the equivalent von Mises stress is the shear stress (Comp. 12 of stress in preferred system). The further stresses are negligible (≈ 10^{-11}).

op/front pp/front/inside a/back/cutside

From the analysis of the components of stress at the MIDDLE SURFACE, the stress that contributes significantly to the evaluation of the equivalent von Mises stress is the shear stress (Comp. 12 of stress in preferred system). The further stresses are negligible (≈ 10^{-11}).

op/front op/front/inside a/back/cutside

From the analysis of the components of stress at the BOTTOM SURFACE, the stress that contributes significantly to the evaluation of the equivalent von Mises stress is the shear stress (Comp. 12 of stress in preferred system). The further stresses are negligible (≈ 10^{-11}).

Thin-walled profile in torsion Opened vs closed cross-section: τ_{12}

Hp) Twist rate: 0.001 rad/mm

In the closed and the opened cases, the stiffness (K_t) evaluated by FE and by the analytical solution are compared, and the relative error has been evaluated as follows:

Error % = $\frac{(FE-Analytical)$ $\frac{m_{i}^{2}-m_{i}}{m_{i}}$ * 100 = $(ratio - 1) * 100$.

The comparison of the stiffness, between the closed and the opened FE models, evidences that:

Error % =
$$
\frac{(opened - Closed)}{closed} * 100 = (ratio - 1) * 100 = -99,84\%.
$$

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Thin-walled profile in torsion Mesh convergence

GOAL:

Open the reference model named torsione rev01 nolabile open vs close .mud two profiles are present, characterized by an opened and a closed section, respectively. They are loaded on the free extremity by an imposed rotation.

Starting from this model, we will compare the influence of the mesh size on the evaluation of torsional stiffness by FE.

The element size under investigation is in the range of [20, 10, 5, 2.5, 1.25] mm

The new models is called torsione rev01 nolabile open vs close convergence.mud

Thin-walled profile in torsion Duplicate Combined

Thin-walled profile in torsion Duplicate Combined

```
| Model 0: avg. element size = 20 mm (reference mesh) --> y-coordinate range [-59, +59]
| Model 1: avg. element size = 10 mm --> y-coordinate range [-259, -141]
| Model 2: avg. element size = 5 mm --> y-coordinate range [-459, -341]
| Model 3: avg. element size = 2.5 mm --> y-coordinate range [-659, -541]
| Model 4: avg. element size = 1.25 mm --> y-coordinate range [-859, -741]
```


Detailed view of the models

Thin-walled profile in torsion Sweep

```
| SWEEP NODES - DUPLICATE DUE TO THE ELEMENTS SUBDIVIDE:
| WITHOUT REMOVING THE LATERAL CRACK OF THE OPENED SECTION (left-hand side models)
| the tolerance (t) must be:
| lower then the crack size (0.1);
| lower than the minimum elements size (1.25);
I therefore t < 0.1| I consider a tolerance value equal to 0.05
*set sweep tolerance
0.05*sweep nodes
all existing
*select clear
| CHECK THE COMMAND PROMPT
| Deleting 42191 duplicate nodes!
| Deleting 0 collapsed elements!
```


Detailed view of the Model_2: RBE2 tied nodes Detailed view of the Model_2: BCs skew-symm

The refinement of the mesh by subdividing the elements required that both the tied nodes of the RBE2, and the nodes involved in the skew-symmetry BCs must be updated.

Make visibile the labels of the RBE2 on the screen, as follows:

PLOT RBE2: SETTING **EX LABELS** REGEN RESET VIEW FILL

As an example, the upload procedure

As an example, the upload procedure adopted for the tied nodes of rbe2_4 is:

The number of tied nodes is function of the mesh refinement.

As an example, the tied nodes of RBE2_4 are 367.

If you adopt the BOX METHOD, keep in mind to remove the retained node of RBE2. The retained node should not be included in the tied nodes, it generates an internal conflict based on the kinematic definition applied to the RBE2.

Keep in mind also to update the skewsymmetry BCs.

After the update of RBE2 and BCs, the Models_2 becomes as shown here. Similarly, this procedure must be accomplished for any models.

The models are ready to be computed.

Thin-walled profile in torsion Mesh Convergence: RESULTS

The stiffness (K_t) evaluated by FE and by the analytical solution are compared, and the relative error has been evaluated as follows:

$$
_\mathsf{Kt_ratio} = \frac{\mathit{Kt_Opened}}{\mathit{Kt_Closed}}.
$$

* exact solution for profile with infinitesimal thickness (t \rightarrow 0)

The influence of the mesh size on the torsional stiffness evalution for closed section is negligible, and it is of limited relevance for the opened section.

Relative error evaluated for the FE models refering to the Model_4.

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Mesh convergence

Critical Aspects: Case A

Mesh Convergence Critical Aspects: Case A

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Mesh Convergence Critical Aspects: Case B

Lamè solution: σ_R| _{r = Ri} = - 5 MPa $\sigma_{\rm C}\vert_{_{\rm r=Ri}}$ = 8.33 MPa

$$
\sigma_r |_{R\text{ int}} = -p_{\text{ int}}
$$

$$
\sigma_c |_{R\text{ int}} = p_{\text{ int}} \frac{R_{\text{est}}^2 + R_{\text{ int}}^2}{R_{\text{est}}^2 - R_{\text{ int}}^2}
$$

Mesh Convergence Critical Aspects: Case B

Mesh Convergence Critical Aspects: Case B

Asymptotic curve of the FE results with respect to the analytical solution.

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Mesh Convergence Critical aspects: singularity occurrence

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LAB Marc Mentat files saved as:

torsione rev01 nolabile.mud torsione rev01 nolabile open vs close.mud torsione rev01 nolabile open vs close mesh convergence.mud

thin walled profile in torsion open vs close.proc thin walled profile in torsion open vs close mesh convergence.proc torsional stiffness evaluation paom2019 v001.ods

Books and papers:

Strozzi, A. (1998). Costruzione di Macchine, Pitagora Editrice, Bologna. Sinclair, G. B. (2004). Stress singularities in classical elasticity–I: Removal, interpretation, and analysis. Applied Mechanics Reviews, 57(4), 251-298. Sinclair, G. B. (2004). Stress singularities in classical elasticity—II: Asymptotic identification. Applied Mechanics Reviews, 57(5), 385-439.

